Pressure tests for gaseous applications in sealed storages: theory and practice

Shlomo Navarro

Abstract
Pressure tests and monitoring devices described in this paper apply to structures destined for gaseous treatments to control principally insects in durable agricultural commodities including cereals. The gaseous treatments included here are: modified atmosphere (MA), controlled atmosphere (CA) and fumigation. These pressure tests are designed to estimate the permissible limits for effectively maintaining the gas composition in small, medium and large size warehouses and silos during the treatment. They are not capable however of measuring gas losses that occur by permeation through structural membranes such as concrete and plastic. Theoretical work to describe the process of gas loss from structures is well documented. This paper reviews essential considerations in measuring gas tightness. However field work to correlate gas tightness to pressure tests are very scarce. The described pressure tests in this paper are applicable for rigid and flexible types of structures. Variable and the constant pressure tests are fully described. In the variable pressure test, time is taken for the pressure to fall between two pressure limits while in the constant pressure test, the flow rate at a given constant pressure is measured. A table is presented for provisional ranges of the variable pressure tests to be applied in structures destined for MA, CA and fumigant treatments.

Introduction
A fundamental requirement for the successful application of gaseous treatments to control stored-product insects is a well-sealed structure. These gaseous treatments include the application of modified atmosphere (MA), controlled atmosphere (CA) and fumigation. In the sealed structure, the desired gas concentration should be maintained at a sufficient level to control insects, whereas otherwise the gas concentration would decrease rapidly without effect. The requirement for gastight storages for application of CA's and MA's appears to be more critical than the requirement for application of fumigants (Bond, 1984). In spite of the trend towards improved sealing of existing silos in some countries (Newman, 1990; Delmenco, 1993), the objective has been either to obtain increased fumigation efficiency, or to convert structures for storage under CA's. To control stored-product insects Jay (1971) recommended a concentration of 60% carbon dioxide (CO₂) in air for 4 days at a temperature of 27°C or above. In the context of MA's, sealed storage of grain termed 'air-tight storage' or 'hermetic storage' is also considered (Hyde, et al., 1973; De Lima, 1990). In the hermetic storage method, the structure should be sufficiently air-tight to enable insects and other aerobic organisms in the grain-mass to reduce oxygen (O₂) concentrations below those permitting insect development.

Fumigants have been used for many years with limited requirements for structural tightness, and covering the grain bulk or the storage under plastic sheets was usually considered satisfactory. Gastightness has for years been a problem for the application of fumigants in storage. The consequences of poorly sealed storages under fumigation should be considered in view of the development of insect resistance to fumigants in poorly sealed structures (Banks and Desmarcheher, 1979; Banks, 1981; Zettler, 1993).

Methods to determine gastightness have been investigated for different purposes. For the analysis of the energy requirements of buildings, air infiltration is a primary source of energy loss and this infiltration can be measured experimentally. CO₂ has also been used experimentally as a tracer gas (Navarro, 1997). Hunt (1980) reviewed some tracer gas techniques to measure air infiltration into buildings and compared fan-pressurization-evacuation procedures to estimate comparative tightness of those structures. The dynamic characteristics of air infiltration into buildings have been studied in order to predict the heating and cooling load of seasonal energy requirements (Hill and Kusuda, 1975). The ASHRAE Handbook of Fundamentals describes the air change method and the crack method in predicting air infiltration rates (Anon., 1972). The crack method or the constant pressure test is usually regarded as more accurate as long as the leak characteristics can be evaluated properly (Hill and Kusuda, 1975). With this method airflow is expressed as:
$Q = b \cdot P^n$

where $Q$ = the volumetric flow rate of air; $b$ = the proportionate constant; $n$ = the exponent and $P$ = the pressure difference exerted on an enclosure.

Meering (1982) investigated a constant pressure test and a variable pressure test for measuring specific silo permeability in silage systems, where the sealed shell is designed to limit entry of $O_2$ to minimize losses in quality. The effect of variations in environmental temperature and atmospheric pressure on $O_2$ intake of silos was simulated, and permeability limits required for proper $O_2$ control in silos containing silage were defined. Gas interchange within freight containers and factors leading to gas interchange between containers and external atmosphere were detailed by Banks et al. (1975). They found that the relationship between applied pressure and gas leak rate gave a useful measure of gastightness. Banks and Anns (1977) developed a practical guide for storage of dry grain under MA and specified requirements for silo gastightness. Their specifications correspond to pressure decay times needed to maintain the atmospheric composition in the silos. Sharp (1982), using the constant pressure test, measured the gastight level of sealed structures. These tests are designed to estimate the permissible limits for effectively maintaining the gas composition in the stores during the treatment.

A decision of the degree of gastightness which is satisfactory or what gas concentrations can be maintained under given environmental and structural conditions should be made prior to the gaseous treatment. This decision should be weighed against the investment involved in sealing a leaky structure to prevent excessive loss of the treatment gas. This paper describes the use of the variable and the constant pressure tests and summarizes provisional recommendations for pressure tests for the successful application of gaseous treatments to control storage insects.

Materials and Methods

Structures for Gaseous Treatments

Pressure tests are applicable for two types of structures: rigid and flexible.

A. Rigid Structures

Rigid structures can withstand the positive pressures exerted on them during the test without changes in volume. Rigid structures may be constructed of concrete, metal or a combination of the two. For CA treatments the structures may be equipped with a pressure relief valve in order to avoid structural failure under extreme and sudden pressure variations.

- Sizes of the rigid structures
  - Small size structures
  - Medium size warehouses and silos
    - Structures in this category may be vertical or horizontal (longer than tall) and the volumes may range between 300 and 2,000 m$^3$. The commodities in store may be stacked in bulk.
  - Large warehouses and silos
    - The warehouse and silo sizes in this category are commonly used as central stores and may range from 2,000 to 10,000 m$^3$ in volume. Single bins of larger sizes are generally less common.

- A general precaution for rigid structures
  - In conducting the pressure tests, care should be taken to carefully monitor the pressure applied, especially with the rigid structures, so as not to exceed the pressure limits this structure can withstand. A small blower used to pressurize the structure can eventually produce enough pressure to cause structural damage. This is particularly important in large stores. It is always advisable to seek the advice of a civil engineer regarding the structural soundness of a storage before conducting pressure tests.

B. Flexible structures

Flexible structures include plastic sheeted structures, bagged stacks sealed in plastic enclosures and bunker type storages. Positive pressures exerted on them cause uncontrolled expansion in volume. Therefore pressure tests in such structures should be performed by creating a negative pressure by evacuation until the sheeting adheres to the commodity or the packed material.

- Size of the flexible structures
  - Small size structures
    - These are mostly destined for indoor gaseous treatments of stacked commodities. The dimensions of the structure are dictated by the manageability of the stack. Sizes of such structures for indoor gaseous treatments can range up to 500 m$^3$ volume.
    - A recent development is to store stacked commodities in fumigatable small flexible structures outdoors using heavy duty liners. They are used for MA storage of stacks of 10–50 tonnes capacity termed storage cubes, and designed for storage at the farmer-cooperative and small trader level (Donahaye et al., 1991).
  - Medium sized flexible structures
    - In this category structures are made from heavy duty material. The flexible silo linings are contained within a circular wall consisting of metal weld mesh. Such structures are fumigatable and suitable for the hermetic storage or MA storage of grain in bulk or in bags and have capacities of up to 1500m$^3$ (Calderon et al., 1989; Navarro and Donahaye, 1993; Navarro et al., 1994; Navarro et al., 1990).
Large size structures

Those are mostly bunker type stores with capacities of 1500 m$^3$ or larger. These bunkers are usually used for bulk storage of commodities. Ramps of concrete, metal or earth, border the bunkers on three sides in order to raise the walls and increase capacity. Before loading the bunkers, the floor and the ramps are lined with plastic sheeting and then an overliner is used as a cover. After loading, the two liners are overlapped and folded to form a hermetic seal, and the over liner is welded closed in order to form a continuous enclosure. Bunker storage for hermetic storage of grain in large bulks of 10,000 to 15,000 tonnes capacity are in current use in Cyprus and Israel (Navarro et al., 1984; Navarro, et al., 1993; Navarro and Donahaye, 1993).

Gas permeation through the rigid structure membrane

Gas loss through the structural membrane during gaseous treatments is an important phenomenon. Membranes of concrete, plaster and plastic liners permit gas permeation and gas exchange. Pressure tests, as described below are not capable of measuring the degree of such losses.

Comparative results with variable pressure test

In variable pressure test, the structure is pressurized to a value above atmospheric, using a fan. The air supply is then shut off and the pressure is allowed to fall by natural leakage to a new value. The time taken to fall from the high (positive or negative) pressure serves as a measure of the degree of sealing. Time elapse to half the pressure is usually considered for comparisons of gas tightness level. A constant static pressure test is more accurate than a variable pressure decay test and has the advantage of being independent of gas volume. However the variable pressure decay test is quicker and therefore the most practical means of measuring gas tightness in grain storage (Anon., 1989; Navarro, 1997; Zahradnik, 1968).

To minimize the thermal influence tests should be carried out preferably before sunrise and in still weather. A pressure of 250 Pa may be taken as an upper limit, but for some structures even this pressure may cause poor seals to open. Welded steel cells and concrete silos may be able to stand 500 Pa, but higher pressures are usually unnecessary.

Comparative tests with variable pressure tests are scarce. Table 1 was prepared as provisional guidelines based on best estimates available in the literature. The suggested times given in Table 1 were doubled for empty storages as an approximation to the intergranular airspace, since for barley, corn, rough rice and wheat, this free space is in the range of 35 to 65% of the total volume (Trvsavusk, 1966).

Banks and Rpp (1984) tested sealed flat storages from 4,500 to 27,000 tonnes capacity and compared the fumigant effectiveness using phosphine with pressure decay time from 150 to 75 Pa. Their tests resulted in successful control of insects when half life pressure decay was 3 min. for the storage capacity of 15,600 and 16,500 tonnes, whereas full insect control could not be achieved when half life pressure decay was less than 1 min for capacities of 4,800 tonnes.

In Table 1 a minimum of 3 mm for large size structures and a minimum of 1.5 mm. for the small range served as basis for half life decay time for full storages.

As a special case for hay fumigation applying methyl bromide (MB), in containers of 12.2 m (40 ft) long pressures from 200 to 100 Pa for a decay time of >10 sec was reported by Ball and van Graver (1997). Although, the minimum 200 g h m$^{-3}$ Ct product was attained using this standard decay time of >10 sec, gas loss was significant.

For exposure times of 12 - 15 h, MB concentration dropped from 58 g m$^{-3}$ to the range of 12 - 18 g m$^{-3}$ and after 22 - 27 h exposure to the range of 10 - 18.5 g m$^{-3}$, pressure halving times ranged from 11 to 85 sec.

With sorptive fumigants like MB, a pressure decay test for the assessment of gas retention is not a precise concept since there are several forces that contribute to the gas loss through the leaks in the structure. Sorption by the treated material is a major cause for drop in gas concentration during the exposure time. Wheat flour treated using MB in experimental jars, resulted in sorption of 70% of the initial gas concentration after 24 h exposure at 25°C (Navarro, 1977). Since the rate of gas loss is independent of leakage from the enclosure, in well sealed structures the overall gas loss rate will approach that expected from sorption only.

For controlled atmosphere storage in Australia, with structures of 300 to 10,000 tonnes capacity, a decay time of 5 min. for an excess pressure drop of 2,500 - 1,500 Pa or 1,500 - 750 Pa or 500 - 250 Pa was regarded satisfactory (Banks et al, 1980). According to Banks and Anns (1980) this range of pressures was chosen so that it is the highest usable without unduly stressing the storage fabric of the store. They commented also that above 10,000 tonnes capacity, pressure testing is difficult to carry out satisfactorily since it requires very stable atmospheric conditions. From analysis of the data presented by Banks et al. (1980) it would appear that for storages with capacities in the range of 1,600 - 1,900 tonnes in CA with an initial CO$_2$ concentration of about 60 - 85% for an average decay time of 11 min, the daily decay rate was about 4% CO$_2$.

With similar range of initial CO$_2$ concentration in a structure of 150 m$^2$ capacity daily gas loss was correlated to different levels of pressure decay times (Navarro et al, 1998). Their comparison resulted in a pressure decay time of 3 min. for a daily decay rate of about 4% CO$_2$.

The influence of hermetic storage on controlling insects was examined using small scale 15, 30 and 52 m$^2$ capacity sealed plastic structures for outdoor storage of wheat,
paddy and corn (Navarro et al., 1995). Pressure decay rates were compared with daily CO₂ decay rates. With these structures successful insect controls were obtained with >1% CO₂ daily decay rate which was found to be equivalent to 5 min. half life pressure decay time. Similarly comparative data was obtained using hermetic bunker storages of about 19,000 m³ capacity, where successful results were obtained when the half life pressure decay was about 9 min. (Navarro et al., 1994).

According to Banks and Annis (1984) daily ventilation rates tolerable in various insect control processes are estimated as 2.6% for hermetic storage, 5% for N₂ based CA, 7% for CO₂ based CA, and 10% for phosphine fumigation. Based on the proportions of ventilation rates, this would account for ventilation rates for fumigation using phosphine being two fold of N₂ based CA, and the latter being as much as twice as hermetic storage. These values were also considered in extrapolating the different ranges given in Table 1.

**Constant pressure tests**

For the constant pressure test a fan, a valve, hosing, a pressure sensor and a gas flow meter (e.g. a Rotameter) is required. The capacity of the flow meter needed varies with the size of the enclosure under test. It is often convenient to make up a series (battery) of flow meters, which gives a range of flow measurements from 0.005 to 3 m³/min. in order to accommodate widely varying requirements and give a wide range of test flows. Alternatively, an electronic thermo-anemometer type flow-meter to cover a wide range of flow may be used. An adjustable rheostat (e.g. Variac) is useful for regulating the speed of the fan if it has a brush motor.

**Test Conditions**

Pressure tests can be performed while the structure contains the stored commodity or when the structure is empty. In both cases the rate of heating or cooling of the structure under test resulting in expansion and contraction of the structure due to ambient climatic conditions, will influence the accuracy of the test. To avoid such situations the tests should be carried out under as stable temperature conditions as possible. With large metal structures it is advisable to perform the tests before sunrise.

It is not advisable to perform pressure tests under windy conditions. Pressure differentials, in addition to those created during the test, may be generated by air entering the structure through leaks. Also, fluctuations in the reference pressure may be excessive under windy conditions. Plot of the natural logarithm of flow rate, lnQ against the natural logarithm of the corresponding pressure, lnP would give a linear relationship. Then the slope (n) and intercept (lnb) of this graph can be calculated and also the flow rate corresponding to a standard equilibrium pressure, e.g. 100 Pa or 250 Pa need to be quoted.

In a detailed study Banks and Annis (1984) presented a model which may be used to calculate the total rate from maximum expected individual contributions of the various phenomena giving rise to gas loss. This model assumes that gas loss from an imperfectly sealed enclosure is largely dependent on the pressure across the leaks in the enclosure fabric and the size and flow characteristics of these leaks. They compared values of the sum of the leak-dependent and of the leak-independent components of ventilation on four types of storage for which the decay time was 5 min. for a pressure difference of 500 to 250 Pa. Ventilation rate was used as a measure of gas interchange rate, alternatively termed as air change rate, or gas loss rate constant. Ventilation produced by wind and temperature variation were considered as leak-dependent major forces. Whereas, diffusion and variation of barometric pressure were considered as negligible forces to cause gas loss. Using the model they attempted to explain why a single pressure test standard to cover all storage structures is inappropriate.

<table>
<thead>
<tr>
<th>Type of gaseous treatment</th>
<th>Structure volume in cubic meters</th>
<th>Variable pressure test decay time (min.) 250 – 125 Pa</th>
<th>Empty Structure</th>
<th>95% Full</th>
</tr>
</thead>
<tbody>
<tr>
<td>Fumigants</td>
<td>Up to 500</td>
<td>3</td>
<td>1</td>
<td>5</td>
</tr>
<tr>
<td></td>
<td>500 to 2,000</td>
<td>4</td>
<td>2</td>
<td></td>
</tr>
<tr>
<td></td>
<td>2,000 to 15,000</td>
<td>6</td>
<td>3</td>
<td></td>
</tr>
<tr>
<td>CA</td>
<td>Up to 500</td>
<td>6</td>
<td>3</td>
<td></td>
</tr>
<tr>
<td></td>
<td>500 to 2,000</td>
<td>7</td>
<td>4</td>
<td></td>
</tr>
<tr>
<td></td>
<td>2,000 to 15,000</td>
<td>11</td>
<td>6</td>
<td></td>
</tr>
<tr>
<td>MA, including airtight storage</td>
<td>Up to 500</td>
<td>10</td>
<td>5</td>
<td></td>
</tr>
<tr>
<td></td>
<td>500 to 2,000</td>
<td>12</td>
<td>6</td>
<td></td>
</tr>
<tr>
<td></td>
<td>2,000 to 15,000</td>
<td>18</td>
<td>9</td>
<td></td>
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</tbody>
</table>

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demonstrated that synoptic variations in barometric pressure played a significant role in air infiltration into the experimental silo. During the experiments synoptic variations in barometric pressure ranging between 11 and 17 Pa/h were observed in the test room. The measured CO₂ concentrations were compared with the calculated values based on equations that took into consideration initial CO₂ adsorption by the wheat, diffusion of CO₂ through the leak, and variations in temperature and barometric pressure. Under experimental conditions, close agreement between the measured and calculated values was obtained.

In view of the work involved in determining the \( n \) value, a rather simplified expression of using the airflow to maintain a constant pressure may be proposed as an alternative. With a similar approach, Banks et al. (1975) used the flow rate at a constant pressure of 125 Pa to correlate with daily gas interchange rate in freight facilities. Such comparative results with constant pressure tests for larger structures and for different gaseous treatments are needed in the literature. Until such information is obtained, provisional decay times for variable pressure test given in Table I may serve as guidelines to determine the suitability of specific storage structures for the successful gaseous control of storage insects.

References


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